

Structural mechanics 2

Summer semester 2023/24

Structural mechanics 2

Lecture no. 8, April 16, 2024

- 1) Moments of inertia
- 2) Mixed moment of inertia
- 3) Radius of gyration, ellipse of inertia

Review – lecture No. 7

Models of structural systems

Model of real structure – numerical model

➤ Simplification, idealization of reality

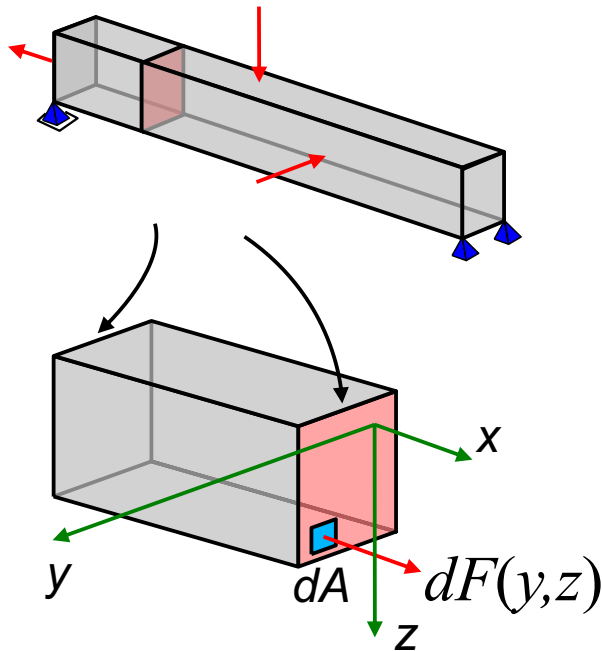
a) Geometry of the structure $\Rightarrow 3D \rightarrow 2D \rightarrow 1D$, division of structure

b) Type of joints, connections, etc. \Rightarrow stiffness  $\begin{matrix} \rightarrow 0 \\ \searrow \\ \rightarrow \infty \end{matrix}$

c) Load \Rightarrow mechanical and non-mechanical load

! The simplification of the structure cannot omit any specific detail and must appropriately represent the structure. !

Normal stress – force equivalency



The load carried by the cross-section is described by internal forces N , V_y , V_z , T , M_y , M_z

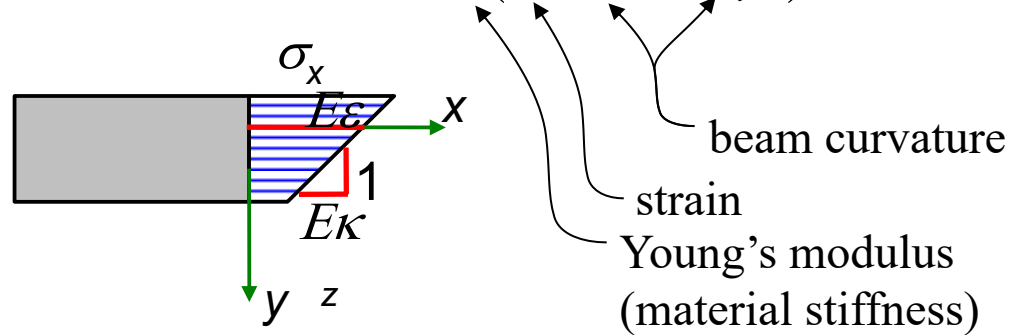
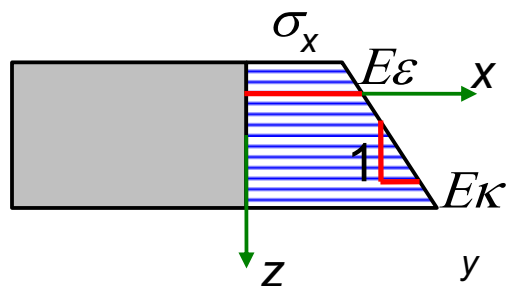
To describe the local force contribution in each point of cross-section the **normal stress** is defined:

$$\sigma_x(y, z) = \frac{dF(y, z)}{dA}$$

Theory of elasticity:

Linear distribution of normal stress over the cross-section:

$$\sigma_x(y, z) = E(\varepsilon - \kappa_z y + \kappa_y z) \quad (1)$$



Normal stress – force equivalency

To be able to calculate the normal stress, we need to determine:

1. Centroid of cross-section (using $S_y = S_z = 0$)
2. Principal axes (using $D_{yz} = 0$)
3. Moments of inertia w.r.t. principal centroidal axes
4. Internal forces w.r.t. principal centroidal axes

Centroid – area

- Limit transition: $m \rightarrow \infty, n \rightarrow \infty \Rightarrow$ fine division

$$A = \lim_{m,n \rightarrow \infty} \sum_{i=1}^m \sum_{j=1}^n \Delta A = \iint_A dA$$

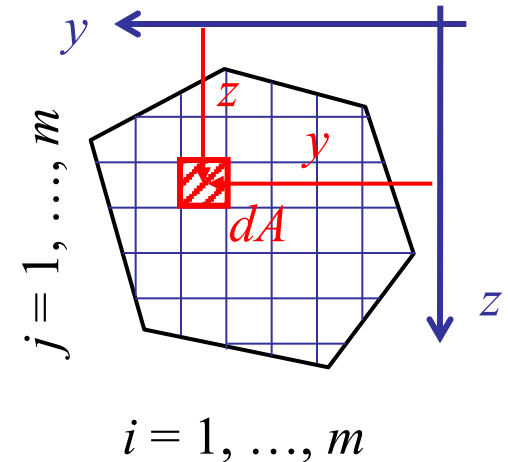
$$S_z = \lim_{m,n \rightarrow \infty} \sum_{i=1}^m \sum_{j=1}^n y_{ij} \Delta A = \iint_A y dA$$

$$S_y = \lim_{m,n \rightarrow \infty} \sum_{i=1}^m \sum_{j=1}^n z_{ij} \Delta A = \iint_A z dA \quad (\text{double integral})$$

- Centroid coordinates (analogous to system of material points):

$$y_c = \frac{\iint_A y \cdot dA}{A} = \frac{S_z}{A}$$

$$z_c = \frac{\iint_A z \cdot dA}{A} = \frac{S_y}{A}$$



Lecture No. 8

Moment of inertia

Mixed moment of inertia

First moment of area

- y axis $S_y = \int_A z dA$ - z axis $S_z = \int_A y dA$ $[m^3]$

Moment of inertia

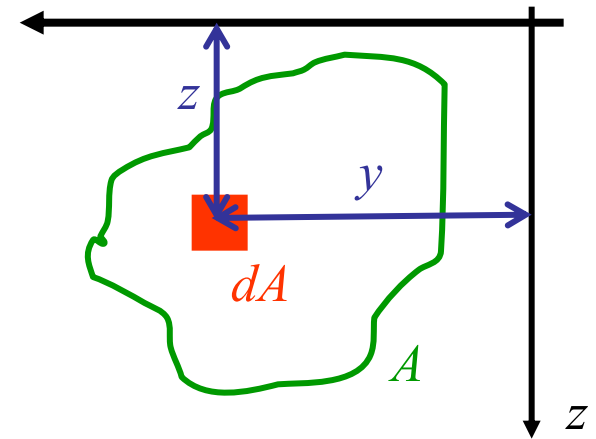
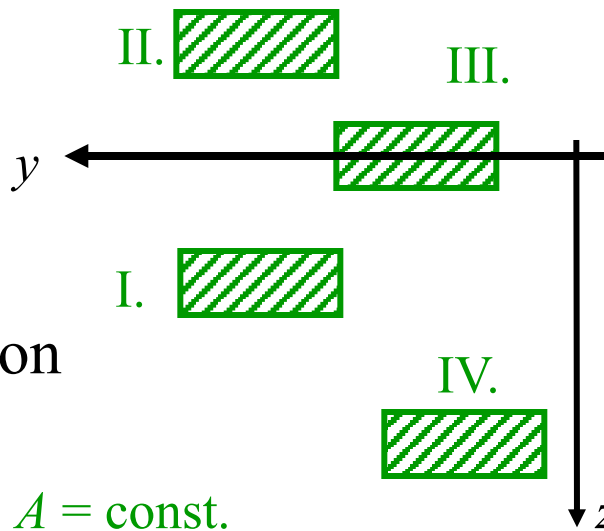
- y axis $I_y = \int_A z^2 dA$ $[m^4]$

- z axis $I_z = \int_A y^2 dA$ $[m^4]$

E.g.:

1) $I_y, I_z > 0$

2) I_y, I_z is dependent on the distance of the area from axis



$$I_y^I = I_y^{II}$$

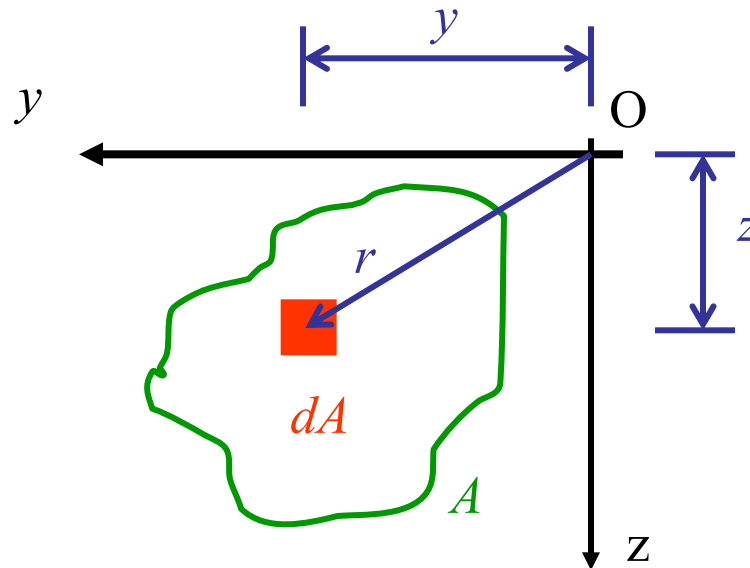
$$I_y^{III} < I_y^I = I_y^{II} < I_y^{IV}$$

Moment of inertia

Mixed moment of inertia

Polar moment of inertia

-w.r.t. origin “O”



$$I_0 = \int_A r^2 dA = \int_A (y^2 + z^2) dA \quad [\text{m}^4]$$

Note: $I_0 = I_z + I_y$

Moment of inertia

Mixed moment of inertia

Mixed moment of inertia

- y, z axes

$$D_{yz} = \int_A yz dA \quad [\text{m}^4]$$

Note:

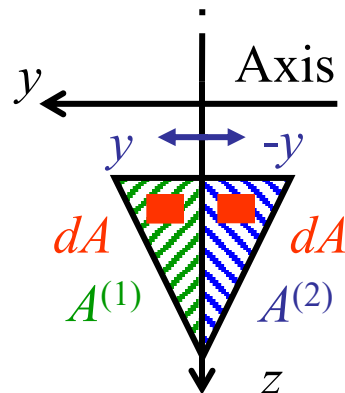
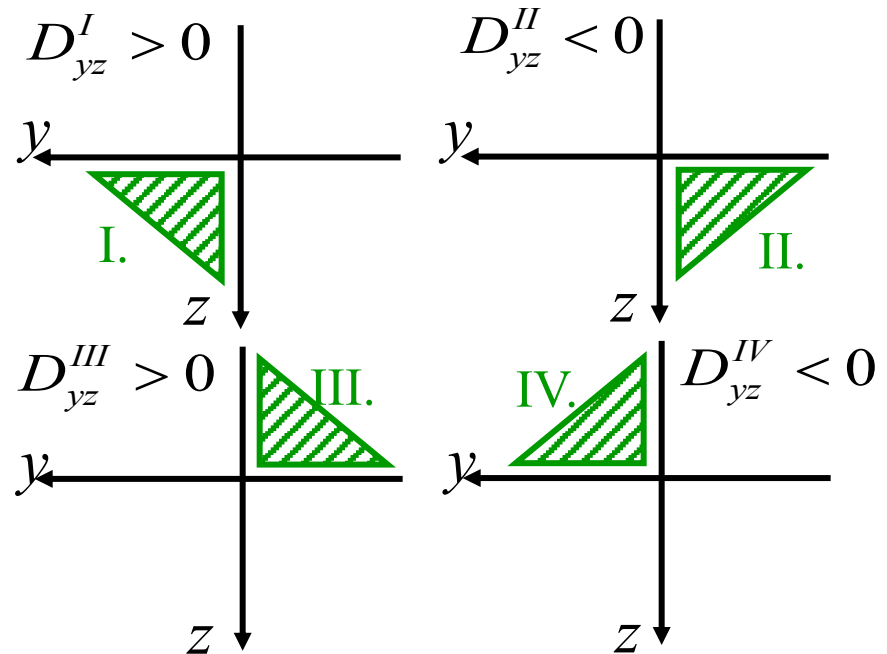
1) $D_{yz} \leq 0$

2) symmetrically placed area

$$D_{yz}^I = -D_{yz}^{II} = D_{yz}^{III} = -D_{yz}^{IV}$$

$$D_{yz}^I > 0$$

3) y or z ... axis of symmetry $\Rightarrow D_{yz} = 0$



$$\int_A yz dA = \int_{A^{(1)}} yz dA + \int_{A^{(2)}} yz dA$$

$$\int_{A^{(1)}} yz dA = - \int_{A^{(2)}} yz dA \Rightarrow D_{yz} = 0$$

Moment of inertia

Mixed moment of inertia

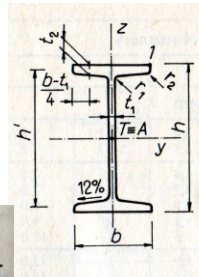
Calculation:

1. Integration

2. Combination of elementary geometric shapes

Statické veličiny

Označení průřezu	A	I_y	W_y	i_y	I_z	W_z	i_z
IE	mm ²	mm ⁴	mm ³	mm	mm ⁴	mm ³	mm
80	610	0,81	20,2	32,3	74,9	3,06	9,8
100	1 200	1,98	39,7	40,6	179	6,49	12,2
120	1 470	3,50	58,4	48,8	279	8,72	13,8
140	1 740	5,72	81,7	57,3	419	11,5	15,5
160	2 020	8,73	109	65,7	586	14,5	17,0
180	2 340	12,9	143	74,2	826	18,4	18,8
200	2 680	18,4	184	82,8	1 150	23,1	20,7
220	3 060	25,5	232	91,3	1 570	28,6	22,7
240	3 480	34,6	289	99,7	1 980	34,5	23,9
270	4 020	50,1	371	112	2 600	41,5	25,4
300	4 650	70,8	472	122	3 370	49,9	26,9
330	5 380	98,4	597	135	4 190	59,9	27,9
360	6 190	133,8	743	147	5 160	71,1	28,9
400	7 140	189,3	947	163	6 660	85,9	30,5
450	8 300	274,5	1 220	182	8 070	101	31,2
500	9 780	392,9	1 570	200	10 400	122	32,6
Násobitel	—	10 ⁶	10 ³	—	10 ³	10 ³	—



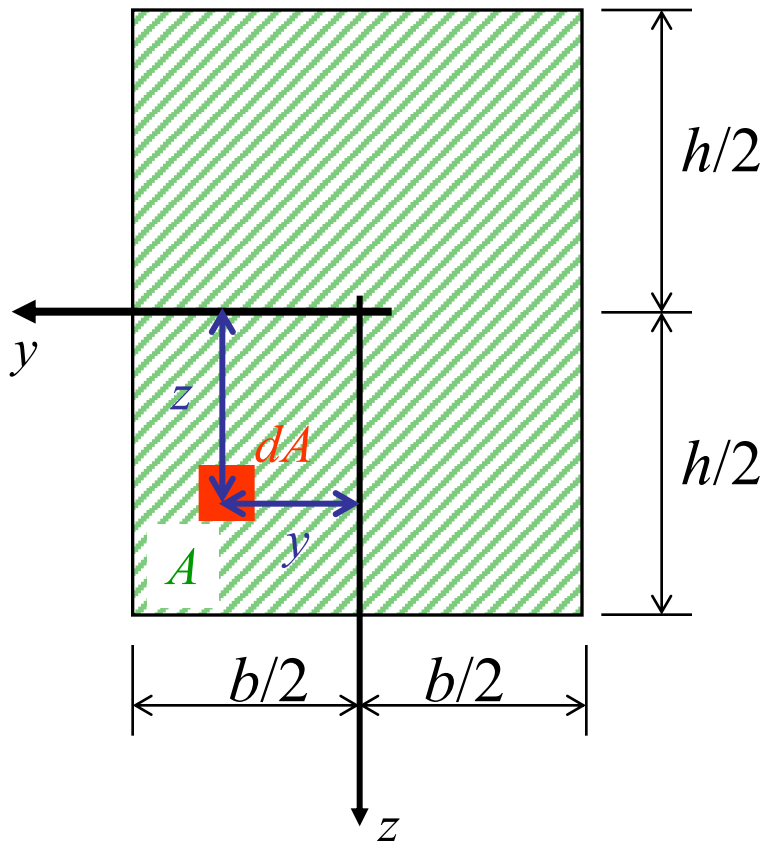
Tvar obrazce	Plocha A	Souřadnice těžiště	Axiální momenty setrvačnosti	Deviační momenty setrvačnosti
	$A = bh$	$w = \frac{b}{2}$ $z = \frac{h}{2}$	$I_{yC} = \frac{bh^3}{12}$, $I_{zC} = \frac{hb^3}{12}$ $I_y = \frac{bh^3}{3}$, $I_z = \frac{hb^3}{3}$	$D_{yCzC} = 0$ $D_{y*z*} = \frac{b^2h^2}{4}$
	$A = \frac{bh}{2}$	$z = \frac{h}{3}$	$I_{yC} = \frac{bh^3}{36}$ $I_y = \frac{bh^3}{12}$ $I_{y*} = \frac{bh^3}{4}$	
	$A = \frac{bh}{2}$	$z = \frac{h}{3}$	$I_{yC} = \frac{bh^3}{36}$, $I_{zC} = \frac{bh^3}{48}$ $I_y = \frac{bh^3}{12}$	$D_{yCzC} = 0$
	$A = \frac{bh}{2}$	$w = \frac{b}{3}$ $z = \frac{h}{3}$	$I_{yC} = \frac{bh^3}{36}$, $I_{zC} = \frac{bh^3}{36}$ $I_y = \frac{bh^3}{12}$, $I_z = \frac{bh^3}{12}$ $I_{y*} = \frac{bh^3}{4}$	$D_{yCzC} = -\frac{b^2h^2}{12}$ $D_{y*z*} = \frac{b^2h^2}{24}$ Znaménko!

(pokračování na další stránce)

Moment of inertia

Mixed moment of inertia

Example: Determine the relation for the moment of inertia w.r.t. centroid axes

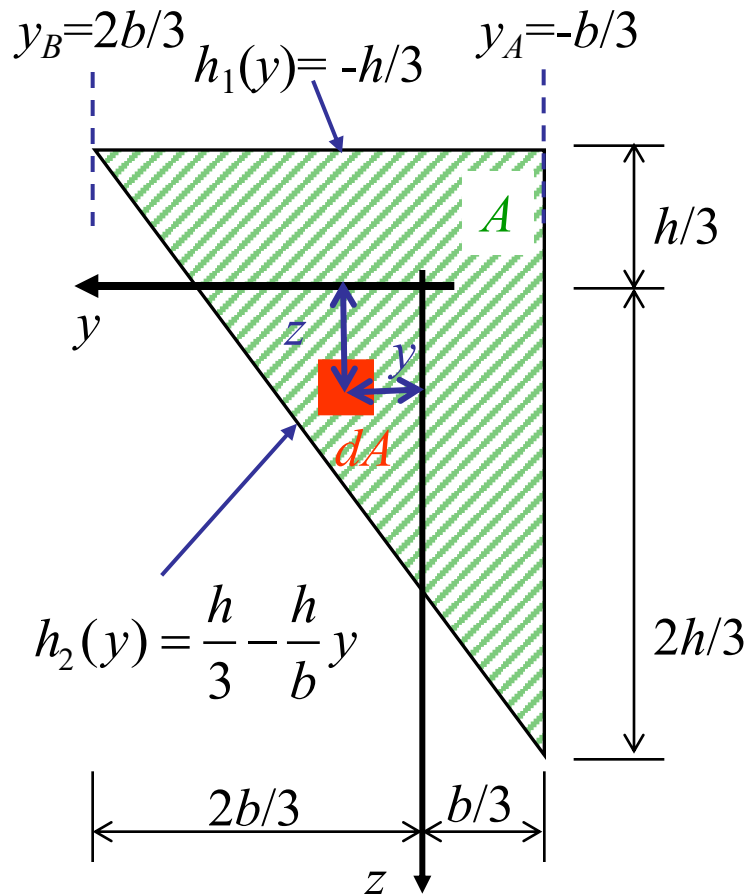


$$\begin{aligned} I_y &= \int_A z^2 dA = \int_{-b/2}^{b/2} \int_{-h/2}^{h/2} z^2 dz dy \\ &= \int_{-b/2}^{b/2} \left[\frac{z^3}{3} \right]_{z=-h/2}^{h/2} dy = \int_{-b/2}^{b/2} \frac{h^3}{12} dy \\ &= \left[\frac{h^3}{12} y \right]_{y=-b/2}^{b/2} = \underline{\underline{\frac{1}{12} b h^3}} \end{aligned}$$

Moment of inertia

Mixed moment of inertia

Example: Determine the relation for the mixed moment of inertia w.r.t. centroid axis

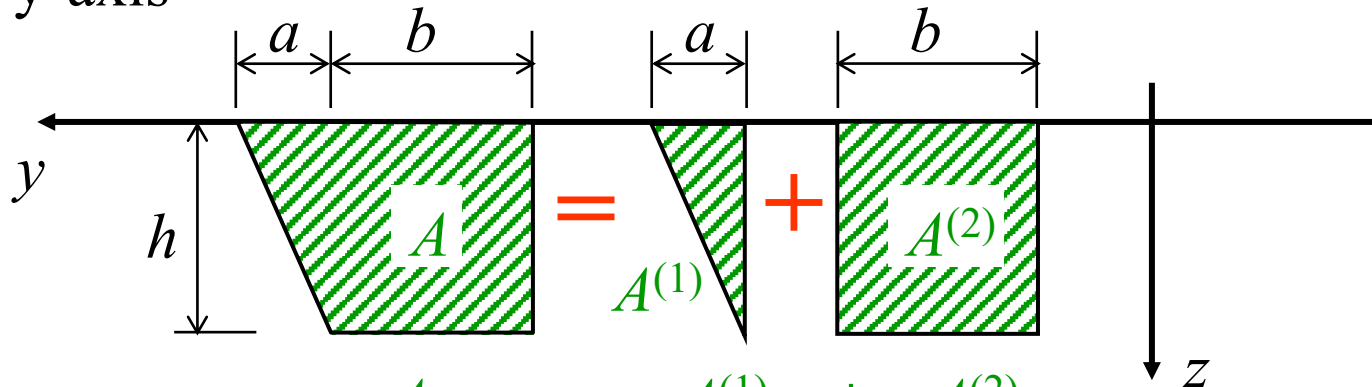


$$\begin{aligned}
 D_{yz} &= \int_A yz \, dA = \int_{y=y_A}^{y_B} \left(\int_{z=h_1(y)}^{h_2(y)} yz \, dz \right) dy \\
 &= \int_{y=-b/3}^{2b/3} \left(\int_{z=-h/3}^{\frac{h}{3} - \frac{h}{b}y} yz \, dz \right) dy = \int_{y=-b/3}^{2b/3} \left(y \left[\frac{z^2}{2} \right]_{z=-h/3}^{\frac{h}{3} - \frac{h}{b}y} \right) dy \\
 &= \int_{y=-b/3}^{2b/3} y \left(\frac{\left(\frac{h}{3} - \frac{h}{b}y \right)^2}{2} - \frac{\left(-\frac{h}{3} \right)^2}{2} \right) dy \\
 &= \left[-\frac{h^2 y^3}{9b} + \frac{h^2 y^4}{8b^2} \right]_{y=-b/3}^{2b/3} = \underline{\underline{-\frac{b^2 h^2}{72}}}
 \end{aligned}$$

Moment of inertia

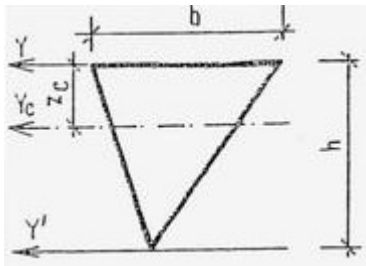
Mixed moment of inertia

Example: Determine the relation for the moment of inertia w.r.t. a given y-axis



$$I_y = \int_A z^2 dA = \int_{A^{(1)}} z^2 dA + \int_{A^{(2)}} z^2 dA = I_y^{(1)} + I_y^{(2)} \quad (\text{split of the integral})$$

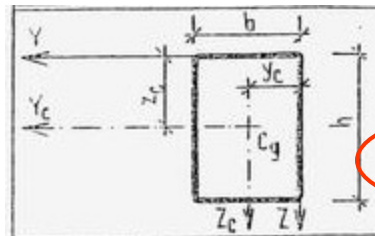
Tabulated values:



$$I_{y_c} = \frac{bh^3}{36}$$

$$I_y = \frac{bh^3}{12}$$

$$I_{y'} = \frac{bh^3}{4}$$



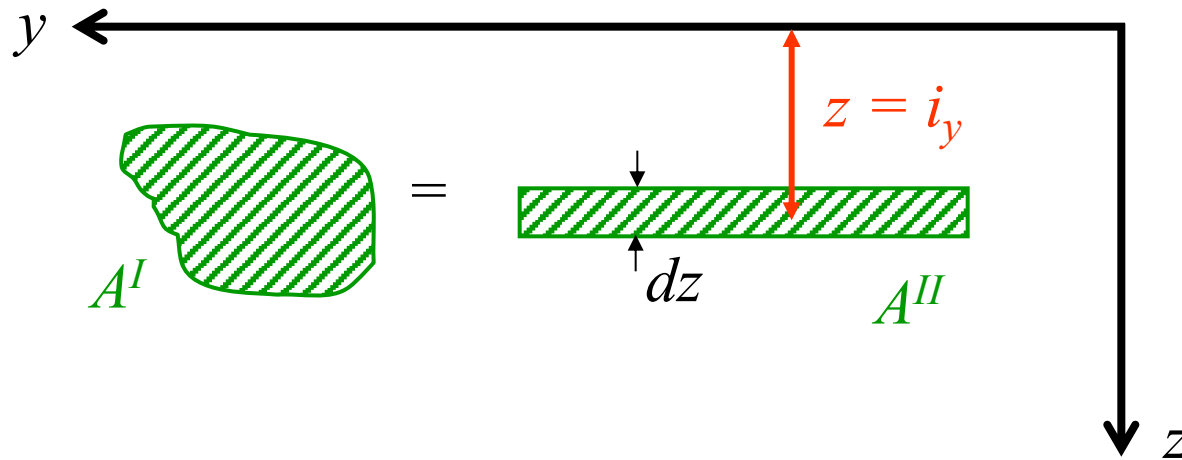
$$I_{y_c} = \frac{bh^3}{12}$$

$$I_y = \frac{bh^3}{3}$$

MoI must be w.r.t. the same axes!!!

$$I_y = \frac{ah^3}{12} + \frac{bh^3}{3}$$

Radius of gyration



Assumption:

$$A^I = A^{II} = A$$

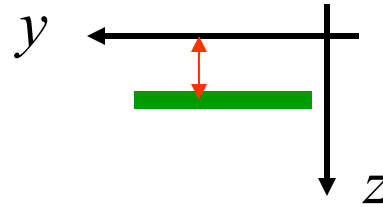
$$I_y^I = I_y^{II} = I_y$$

It is valid that: $I_y^{II} = \int_{A^{II}} z^2 dA = i_y^2 \cdot A^{II}$ ($z = \text{const.} = i_y$)

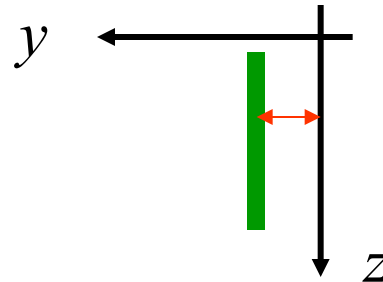
$$\Rightarrow I_y = i_y^2 \cdot A$$

Radius of gyration

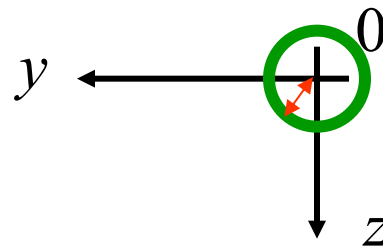
- y axis: $i_y = \sqrt{\frac{I_y}{A}}$



- z axis: $i_z = \sqrt{\frac{I_z}{A}}$



- w.r.t. 0 : $i_0 = \sqrt{\frac{I_0}{A}}$



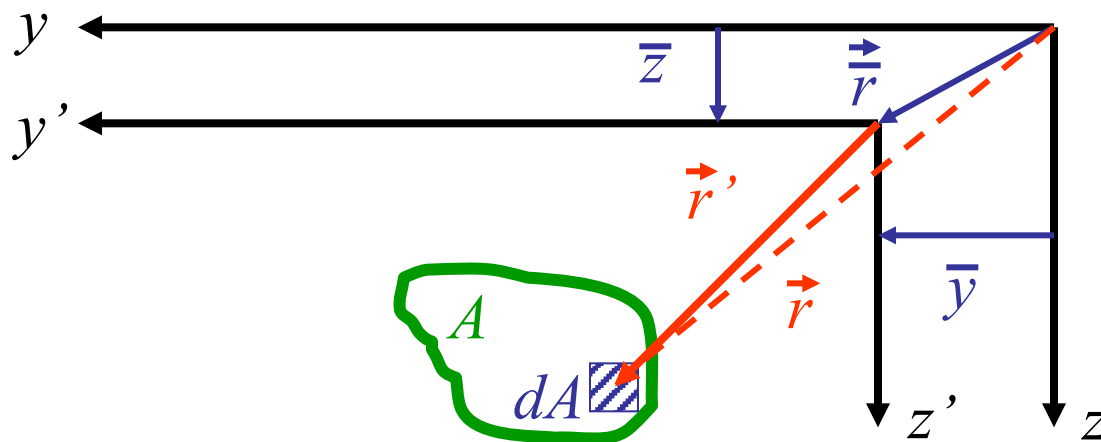
Note: i_y, i_z, i_0 [m]

$$i_0^2 = i_y^2 + i_z^2$$

Transformation – translation

Moment of inertia w.r.t. translated axes

Moments of inertia and mixed moment of inertia w.r.t. y, z axis are known, determine these moments w.r.t. y', z' axes.



Transformation of coordinates

$$y' = y - \bar{y}$$

$$z' = z - \bar{z}$$

$$(\vec{r}' = \vec{r} - \vec{r})$$

$$I_{z'} = \int_A y'^2 dA = \int_A (y - \bar{y})^2 dA = \int_A y^2 dA - 2\bar{y} \int_A y dA + \bar{y}^2 \int_A dA$$

$$= \underline{I_z - 2\bar{y}S_z + \bar{y}^2 A}$$

Note: $\bar{y} = \text{const.}$

Transformation – translation

Using similar approach we get:

$$I_{y'} = I_y - 2\bar{z} S_y + \bar{z}^2 A$$

$$I_{0'} = I_0 - 2\bar{y} S_z - 2\bar{z} S_y + A(\bar{y}^2 + \bar{z}^2)$$

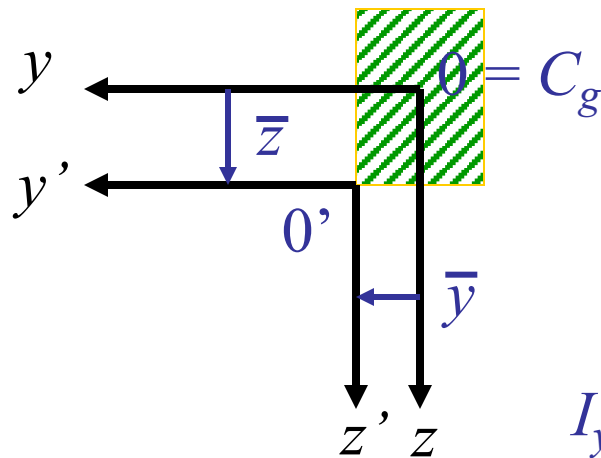
$$D_{y'z'} = D_{yz} - \bar{y} S_y - \bar{z} S_z + \bar{y}\bar{z} A$$

Note:

$$I_{0'} = I_{y'} + I_{z'}$$

Transformation – translation (ver. 1)

If the origin of CS is placed into the center of gravity then $S_y = S_z = 0$



$$\begin{pmatrix} y_c = \frac{S_z}{A} = 0 \\ z_c = \frac{S_y}{A} = 0 \end{pmatrix}$$

$I_y, I_z, D_{yz}, I_0 \dots$ moments of inertia and mixed moment of inertia w.r.t. **centroid CS**

$$I_{y'} = I_y + \bar{z}^2 A$$

$$D_{y'z'} = D_{yz} + \bar{y} \bar{z} A$$

$$I_{z'} = I_z + \bar{y}^2 A$$

$$I_{0'} = I_0 + (\bar{y}^2 + \bar{z}^2) A$$

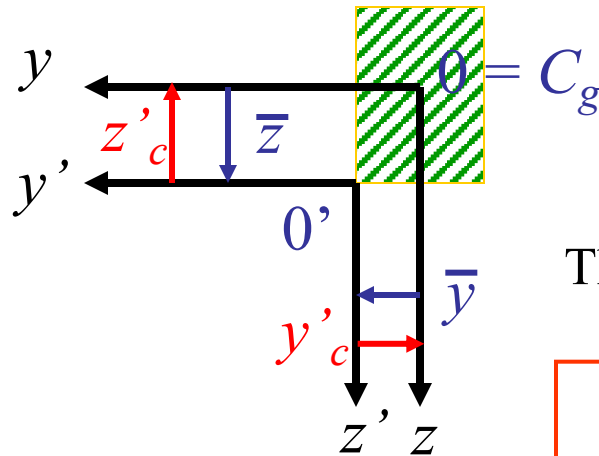
(Steiner's theorem)

Transformation – translation (ver. 2)

If the origin of CS is placed into the center of gravity then $S_y = S_z = 0$

If:

$$\begin{aligned} y'_c &= -\bar{y} \\ z'_c &= -\bar{z} \end{aligned}$$



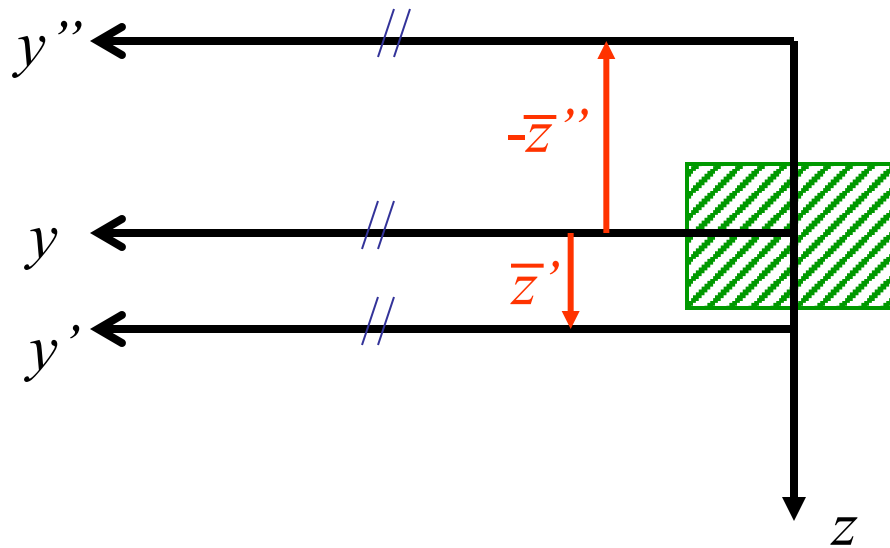
Then the Steiner theorem can be also written as:

$$\begin{aligned} I_{y'} &= I_y + \bar{z}^2 A = I_y + z'^2_c A \\ I_{z'} &= I_z + \bar{y}^2 A = I_z + y'^2_c A \\ D_{y'z'} &= D_{yz} + \bar{y} \bar{z} A = D_{yz} + y'_c z'_c A \\ I_{O'} &= I_0 + (\bar{y}^2 + \bar{z}^2) A = I_0 + (y'^2_c + z'^2_c) A \end{aligned}$$

(Steiner's theorem)

Transformation – translation

Note:



$$I_{y'} = I_y + \bar{z}'^2 A$$

$$I_{y''} = I_y + (-\bar{z}'')^2 A$$

$$|\bar{z}'| < |\bar{z}''| \Rightarrow$$

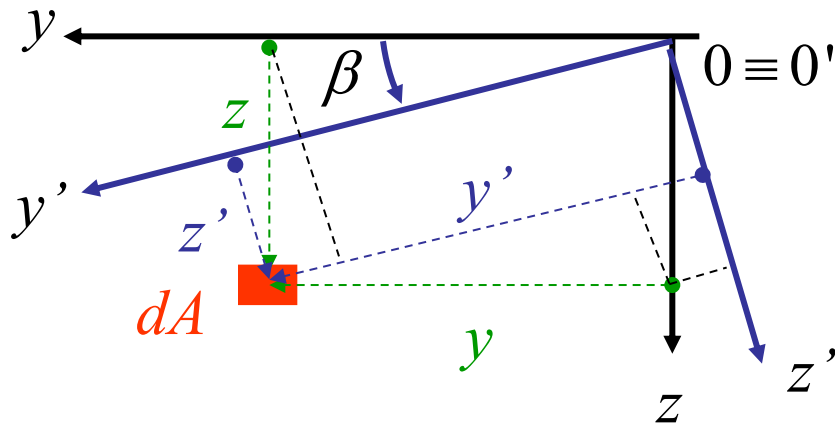
$$I_y < I_{y'} < I_{y''}$$

... the moment of inertia w.r.t. centroid axis has **the smallest value**.

Transformation – rotation

Moment of inertia w.r.t. rotated axes

Moments of inertia and mixed moment of inertia w.r.t. y, z axis are known, determine these moments w.r.t. y', z' axes.



Transformation of coordinates:

$$y' = y \cdot \cos \beta + z \cdot \sin \beta$$

$$z' = -y \cdot \sin \beta + z \cdot \cos \beta$$

$$\{r'\} = \{T\} \{r\}$$

$$\begin{aligned} I_{z'} &= \int_A y'^2 dA = \int_A (y \cdot \cos \beta + z \cdot \sin \beta)^2 dA \\ &= \cos^2 \beta \cdot \underbrace{\int_A y^2 dA}_{I_z} + \underbrace{2 \sin \beta \cos \beta}_{\sin 2\beta} \underbrace{\int_A yz dA}_{D_{yz}} + \sin^2 \beta \underbrace{\int_A z^2 dA}_{I_y} \\ &= I_y \sin^2 \beta + I_z \cos^2 \beta + D_{yz} \sin 2\beta \end{aligned}$$

Transformation – rotation

Using similar approach we get:

$$I_{y'} = I_y \cos^2 \beta + I_z \sin^2 \beta - D_{yz} \sin 2\beta$$

$$D_{y'z'} = \frac{1}{2} (I_y - I_z) \sin 2\beta + D_{yz} \cos 2\beta$$

Note: this transformation is valid for any CS (not only centroid CS)

Transformation – rotation

$$\begin{aligned} I_{O'} &= \underline{I_{y'}} + I_{z'} = (I_y + I_z)(\cos^2 \beta + \sin^2 \beta) + \sin 2\beta (D_{yz} - D_{yz}) \\ &= \underline{I_y + I_z} = I_O \end{aligned}$$

Matrix notation:

$$\begin{bmatrix} I_{y'} & -D_{y'z'} \\ -D_{y'z'} & I_{z'} \end{bmatrix} = \begin{bmatrix} \cos \beta & \sin \beta \\ -\sin \beta & \cos \beta \end{bmatrix} \begin{bmatrix} I_y & -D_{yz} \\ -D_{yz} & I_z \end{bmatrix} \begin{bmatrix} \cos \beta & -\sin \beta \\ \sin \beta & \cos \beta \end{bmatrix}$$

$$[I'] = [T][I][T]^T$$

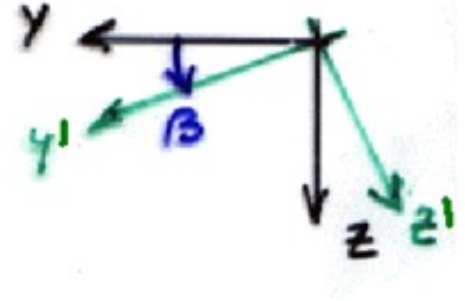
$[I']$, $[I]$... inertia tensor

$[T]$... transformation tensor

Transformation – rotation

Invariants of inertia tensor

Invariant = its value does not change when arbitrary rotations are applied



Linear invariant:

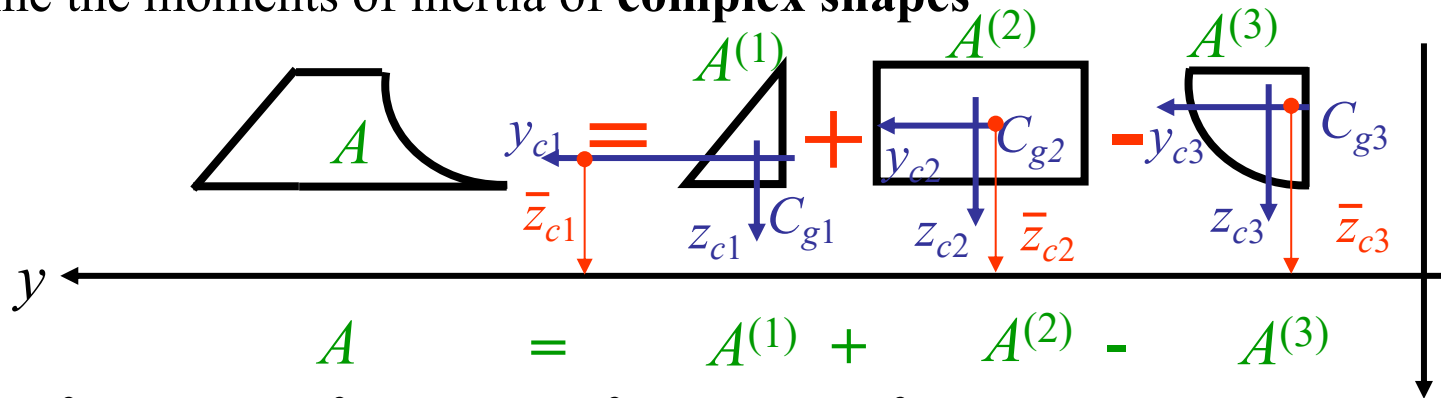
$$I_{1I} = I_y + I_z = I_{y'} + I_{z'} = I_0$$

Quadratic invariant:

$$I_{2I} = I_y I_z - D_{yz}^2 = I_{y'} I_{z'} - D_{y'z'}^2$$

Transformation – example

Determine the moments of inertia of **complex shapes**



$$A = A^{(1)} + A^{(2)} - A^{(3)}$$

$$I_y = \int_A z^2 dA = \int_{A^{(1)}} z^2 dA + \int_{A^{(2)}} z^2 dA - \int_{A^{(3)}} z^2 dA$$

$$= I_y^{(1)} + I_y^{(2)} - I_y^{(3)} \quad (\text{Note: all w.r.t. } y \text{ axis!})$$

$$I_y^{(1)} = \underbrace{I_{y_{c1}}^{(1)}} + A^{(1)} \underbrace{\bar{z}_{c1}^2}$$

Coordinates of origin of y, z axes
(w.r.t y_{ci}, z_{ci} axes)

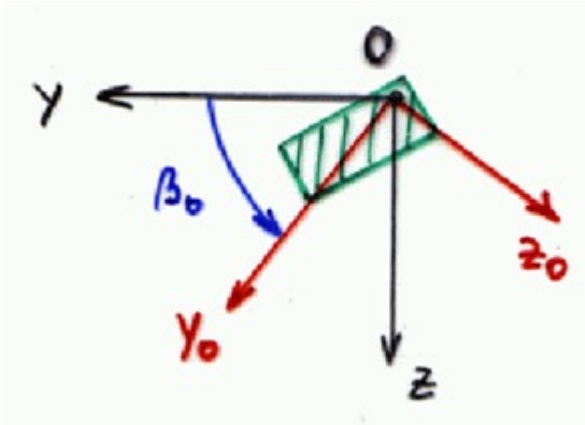
$$I_y^{(2)} = \underbrace{I_{y_{c2}}^{(2)}} + A^{(2)} \underbrace{\bar{z}_{c2}^2}$$

$$I_y^{(3)} = \underbrace{I_{y_{c3}}^{(3)}} + A^{(3)} \underbrace{\bar{z}_{c3}^2}$$

Moments of inertia w.r.t. centroids of individual areas; e.g. tabulated value

Moment of inertia – principal axes

For a given origin “O” we seek the extreme values of moments of inertia => **principal axis**



$$\begin{aligned}\frac{dI_{y'}}{d\beta} &= (I_z - I_y) \sin 2\beta - 2D_{yz} \cos 2\beta \\ &= -\frac{dI_{z'}}{d\beta}\end{aligned}$$

$$\frac{dI_{y'}}{d\beta} = 0 \Rightarrow \tan 2\beta_0 = \frac{2D_{yz}}{I_z - I_y}$$

$$\frac{dI_{z'}}{d\beta} = 0 \quad \Rightarrow$$

principal axis of inertia

Moment of inertia – principal axes

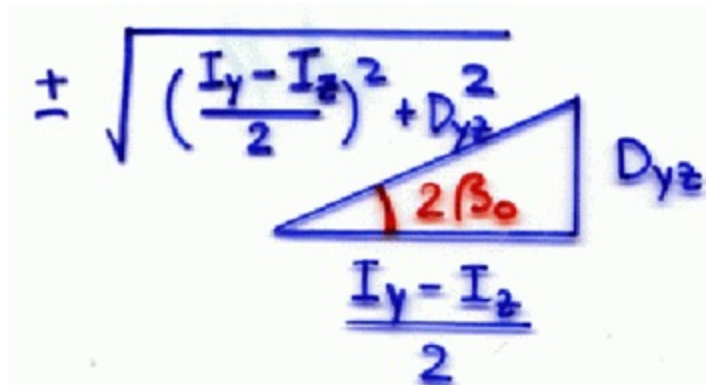
Principal moments of inertia

$$I_{y_0} = I_y \cos^2 \beta_0 + I_z \sin^2 \beta_0 - D_{yz} \sin 2\beta_0$$

$$I_{z_0} = I_y \sin^2 \beta_0 + I_z \cos^2 \beta_0 + D_{yz} \sin 2\beta_0$$

$$\cos^2 \beta_0 = \frac{1}{2} (\cos 2\beta_0 + 1); \quad \sin^2 \beta_0 = \frac{1}{2} (1 - \cos 2\beta_0);$$

$$I_{y_0} = \frac{I_y + I_z}{2} + \frac{I_y - I_z}{2} \cos 2\beta_0 - D_{yz} \sin 2\beta_0$$



$$\cos 2\beta_0 = \frac{I_y - I_z}{2 \sqrt{\left(\frac{I_y - I_z}{2}\right)^2 + D_{yz}^2}}$$

$$\sin 2\beta_0 = \dots$$

Moment of inertia – principal axes

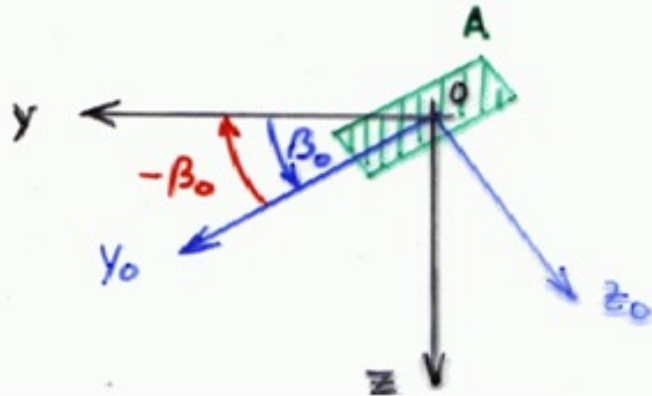
$$\left. \begin{aligned} I_{y0} &= \frac{I_y + I_z}{2} \pm \sqrt{\left(\frac{I_y - I_z}{2}\right)^2 + D_{yz}^2} \\ I_{z0} &= \frac{I_y + I_z}{2} \mp \sqrt{\left(\frac{I_y - I_z}{2}\right)^2 + D_{yz}^2} \end{aligned} \right\} \begin{array}{l} \text{Principal} \\ \text{moments} \\ \text{of inertia} \\ I_{1,2} \ (I_1 \geq I_2) \end{array}$$

$$D_{y_0 z_0} = 0$$

Note:

$$\begin{array}{ll} I_y + I_z & \dots \text{ first invariant} \\ \sqrt{\left(\frac{I_y - I_z}{2}\right)^2 + D_{yz}^2} & \dots \text{ must be independent} \\ & \text{on the rotation of CS} \end{array}$$

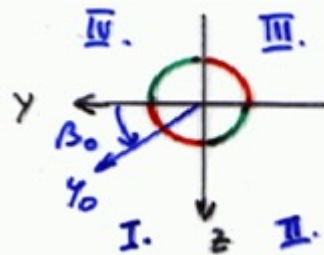
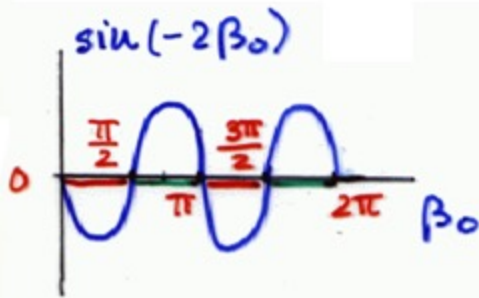
Moment of inertia – principal axes



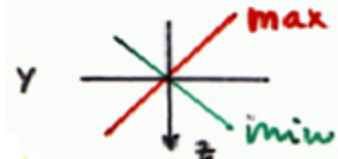
Transformation $(y_0, z_0) \rightarrow (y, z)$

$$D_{yz} = \frac{1}{2} (I_{y_0} - I_{z_0}) \sin(-2\beta_0)$$

> 0	$I_{y_0} > I_{z_0}$	> 0	II., IV.
> 0	$I_{z_0} > I_{y_0}$	< 0	I., III.
< 0	$I_{z_0} > I_{y_0}$	> 0	II., IV.
< 0	$I_{y_0} > I_{z_0}$	< 0	I., III.
	↑	↑	
	I_1	I_2	

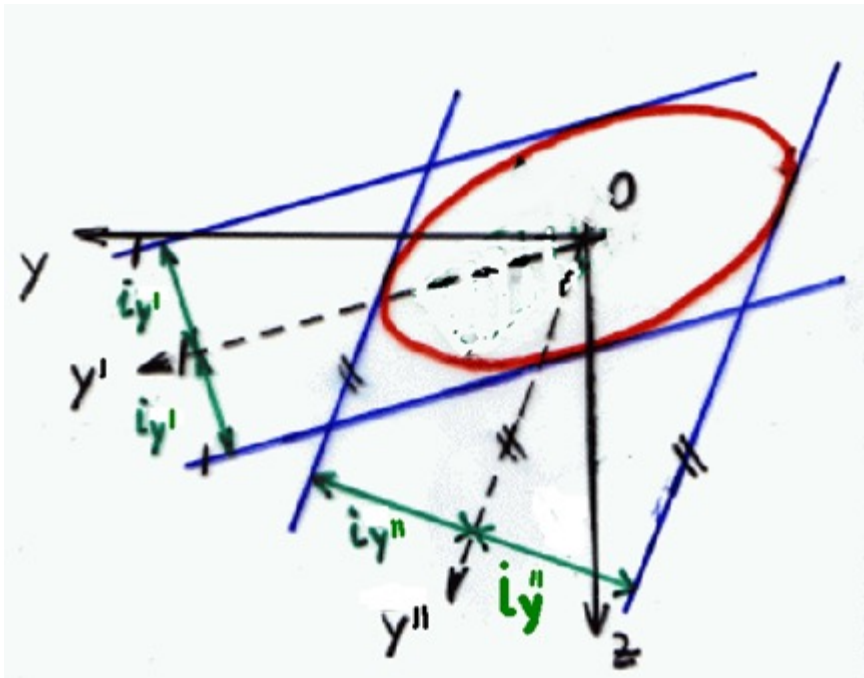


$D_{yz} > 0 \Rightarrow$ axis of max. moment is in interval II. and IV.



$D_{yz} < 0 \Rightarrow$ axis of max. moment is in interval I. and III.

Ellipse of inertia



Lines with the distance equal to the corresponding radius of gyration ($i_y, i_{y'}, i_{y''}, \dots$) are drawn parallel to the axis of inertia

These lines are tangents to the **ellipse of inertia**

Note:

$$i_{y'} = \sqrt{\frac{I_{y'}}{A}}$$

Ellipse of inertia

Equation of ellipse of inertia:

$$I_y y^2 + I_z z^2 - 2D_{yz} yz = \frac{I_y I_z - D_{yz}^2}{A}$$

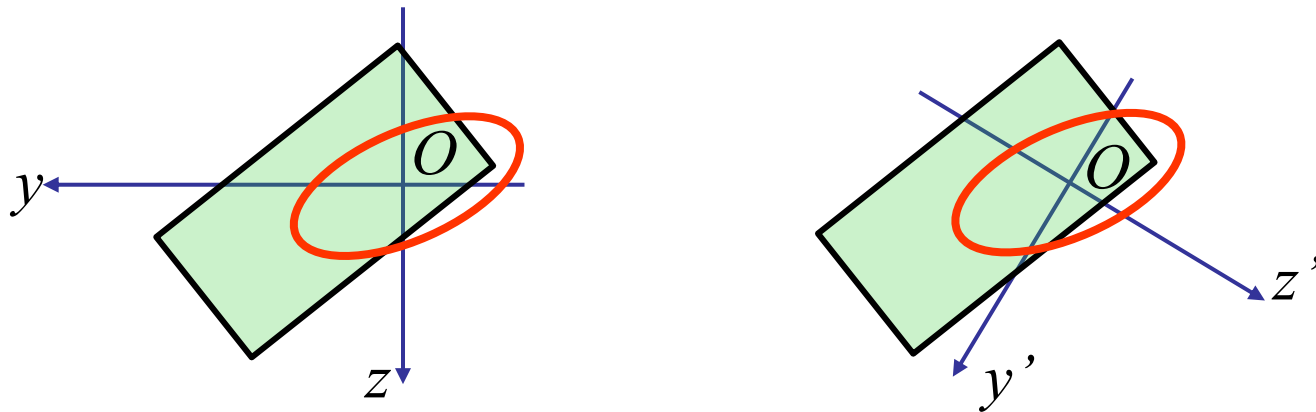
This equation can be written in the form:

$$\{y, z\} \begin{bmatrix} I_y & -D_{yz} \\ -D_{yz} & I_z \end{bmatrix} \begin{Bmatrix} y \\ z \end{Bmatrix} = \frac{I_y I_z - D_{yz}^2}{A} \quad \mathbf{I_{20} \text{ invariant}}$$

Ellipse of inertia

It can be shown by means of the transformation relations that for two coordinate systems rotated against each other we can write:

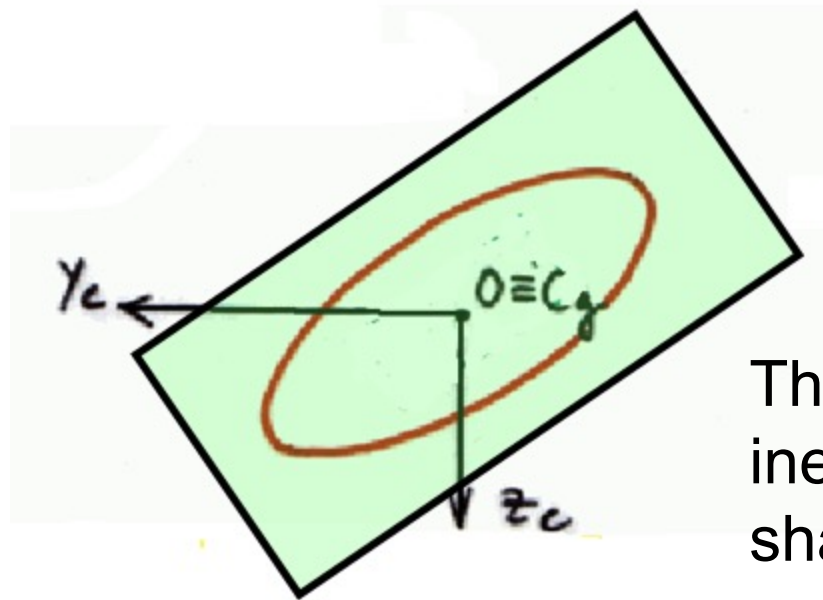
$$\{y, z\} \begin{bmatrix} I_y & -D_{yz} \\ -D_{yz} & I_z \end{bmatrix} \begin{Bmatrix} y \\ z \end{Bmatrix} = \{y', z'\} \begin{bmatrix} I_{y'} & -D_{y'z'} \\ -D_{y'z'} & I_{z'} \end{bmatrix} \begin{Bmatrix} y' \\ z' \end{Bmatrix}$$



Therefore, the shape of ellipse of inertia does not depend on the rotation of coordinate system but only on the shape of the cross-section and the position of origin “O”

Central ellipse of inertia

If the origin of CS coincides with the center of gravity
=> **central ellipse of inertia**



The shape of ellipse of inertia partly follows the shape of cross-section

Central ellipse of inertia

Equation of central ellipse of inertia:

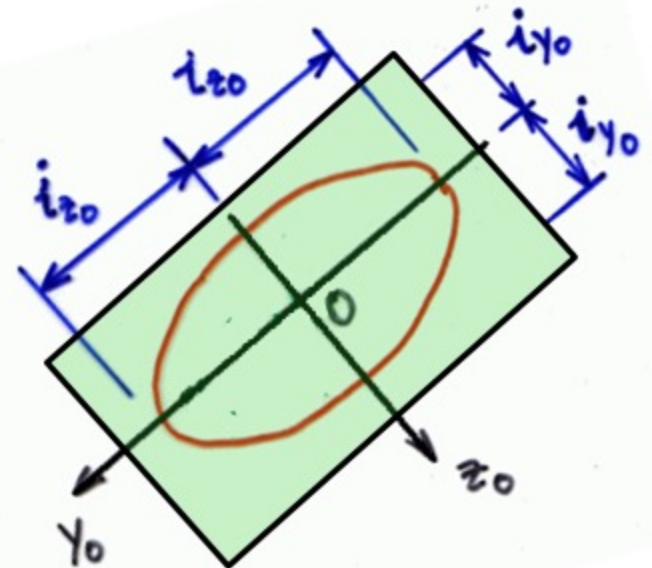
$$I_{y_0}y_0^2 + I_{z_0}z_0^2 - 0 = \frac{I_{y_0}I_{z_0} - 0}{A} \quad / \cdot \frac{A}{I_{y_0}I_{z_0}}$$

$$\frac{A}{I_{z_0}}y_0^2 + \frac{A}{I_{y_0}}z_0^2 = 1$$

$$\frac{y_0^2}{i_{z_0}^2} + \frac{z_0^2}{i_{y_0}^2} = 1$$

i_{y_0}, i_{z_0} ... ellipse semi-axes

y_0, z_0 ... principal axes of ellipse of inertia



The End